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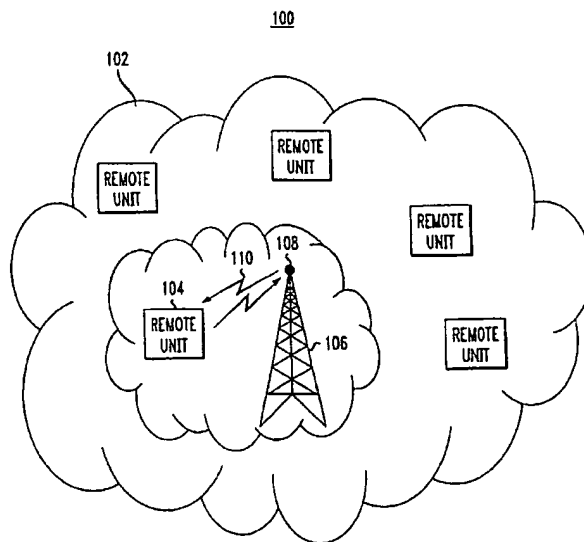
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(54) Title: **METHODS AND APPARATUS FOR USE IN REDUCING RESIDUAL PHASE ERROR IN OFDM COMMUNICATION SIGNALS**



(57) Abstract: Methods and apparatus for use in reducing residual phase error (RPE) in orthogonal frequency division multiplexed (OFDM) communication signals are described. One method includes the steps of calculating a phase of each one of a plurality of channel-compensated data symbols to generate a plurality of data symbols phases; performing a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols to generate a plurality of information symbol phases; calculating a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences; and determining a residual phase error based on the plurality of phase differences.

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METHODS AND APPARATUS FOR USE IN REDUCING RESIDUAL
PHASE ERROR IN OFDM COMMUNICATION SIGNALS

BACKGROUND OF THE INVENTION

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1. Field of the Invention

The present invention relates generally to the field of radio communication receivers. More particularly, the present invention relates to the field of reducing residual phase error (RPE) of orthogonal frequency
10 division multiplexing (OFDM) signals in OFDM communication receivers.

2. Description of the Related Art

An increasing need for broadband mobile/fixed wireless communications services has motivated researchers and radio engineers to
15 search for a variety of feasible radio airlink interface techniques for such wireless communication systems. An airlink interface technique based on the Orthogonal Frequency Division Multiplexing (OFDM) modulation is considered an attractive candidate for a broadband wireless transmission system due to its spectral efficiency, its robustness in different multipath
20 propagation environments and its ability to combat intersymbol interference (ISI).

OFDM is a multi-carrier modulation method. It divides an entire frequency band into many, say N , subchannels or frequency tones, and each subchannel is modulated with a constellation symbol to be
25 transmitted. In its application as a multiple access method for a point-to-multipoint wireless communication system, OFDM arranges these total N subchannels as follows. M adjacent subchannels are grouped together (where $M \ll N$) without overlapping between adjacent groups. Each mobile user is assigned a cluster of M subchannels when it needs to
30 transmit information data between its serving base station and its

terminal. In each cluster of M subchannels assigned to an individual user, one or more subchannels may be used to transmit pilot signals and are called "pilot subchannels." The rest of the subchannels bear information data and are called "information subchannels." For an available
5 bandwidth of B MHz, there are total of N subchannels with a frequency space of B/N MHz; this band can simultaneously support N/M users.

An OFDM-based wireless system, however, is very sensitive to channel phase errors and the phase noise of the receiver local oscillator (LO). Therefore, an effective fading channel estimation and the transform
10 domain channel compensation become necessary to restore OFDM signal orthogonality, to correct phase error, and to conduct coherent demodulation in the receiver.

Pilot symbol-aided approaches are widely used to estimate the fading channel properties which corrupt the transmitted signal. In an
15 OFDM/TDMA system, an OFDM data block is the block of M constellation symbols to be transmitted within a TDMA time slot. When the transmission channel or phase noise changes significantly from one OFDM data block to the next, channel estimation and transform domain channel compensation must be performed in each individual data block
20 with the pilot symbols inserted in the given data block. For example, the interval between two OFDM data blocks may be on the order of 3-5 milliseconds. In such a relatively long time period, the phase noise effect of the receiver LO may change significantly.

Co-channel interference due to any frequency reuse pattern, multipath fading, and additive white Gaussian noise (AWGN) are primary
25 constraints to an acceptable performance in a cellular/wireless communication system. In addition, intercarrier interference (ICI) due to channel variation and phase noise always exists in an OFDM-based wireless system. Thus, the pilot symbols as well as the information
30 symbols are corrupted by co-channel interference, intercarrier-

interference, noise, and other channel impairments. All of these impairments in the received pilot signals significantly affect the accuracy of the channel estimation. A residual phase error (RPE) is the phase error that remains after the received constellation symbols are compensated
5 based on an inaccurate channel estimation.

With conventional techniques, the accuracy of the channel estimation may be improved by either increasing the number of pilot signals and/or increasing their transmission power. On one hand, using a larger number of pilot symbols results in a higher transmission overhead
10 and hence a lower system capacity. On the other hand, a larger transmission power for pilot sub-channels results in larger ICIs for information-bearing tones and hence causes implementation difficulties. Accordingly, there is an existing need to reduce the residual phase error in OFDM communication signals without the deficiencies of the prior art.

15

SUMMARY OF THE INVENTION

Methods and apparatus for use in reducing the residual phase error (RPE) in OFDM communication signals are described. A pilot symbol-aided channel estimation scheme is employed in a wireless OFDM system.
20 The new technique takes advantage of OFDM-based systems where a block of constellation symbols are transmitted simultaneously and all of these symbols experience the same channel fading. Broadly, the technique utilizes a block of detected symbols, based on their hard-decisions as the real transmitted symbols, to estimate and remove the residual phase error
25 after the channel has been compensated.

The method of the preferred embodiment includes the steps of generating a plurality of channel-compensated data symbols by performing channel compensation on OFDM communication signals using one or more pilot tones; calculating a phase of each one of the plurality of
30 channel-compensated data symbols to generate a plurality of data symbol

phases; performing a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols; calculating a phase of each one of the plurality of information symbols to generate a plurality of information symbol phases; and
5 calculating a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences. The preferred method may include the further steps of selecting a subset of phase differences from the plurality of phase differences that does not include one or more of the largest values in the
10 plurality of phase differences; using the subset of phase differences to generate an average phase difference; determining a residual phase error based on the average phase difference; and correcting phases of channel compensated data symbols based on the residual phase error.

15 **BRIEF DESCRIPTION OF THE DRAWINGS**

FIG. 1 is a diagram of a wireless communication system, such as a fixed wireless system utilizing orthogonal frequency division multiplexing (OFDM) communication techniques, which includes one or more base units and one or more remote units;

20 FIG. 2 is a general block diagram of processing components for an OFDM-based wireless communication system which utilizes pilot-based signal correction;

FIG. 3 is a block diagram of more specific processing components of the remote unit of FIG. 2 related to channel compensation using pilot
25 tone symbols;

FIG. 4 is a graph showing relationships between fading channel gain, its estimation, and the estimation error for the channel compensation described in relation to FIG. 3;

FIG. 5 is a block diagram of a first embodiment of components utilized in the remote unit of FIG. 2 which are operative to reduce residual phase error in OFDM communication signals;

FIG. 6 is a block diagram of a second embodiment of components
5 utilized in the remote unit of FIG. 2 which are operative to reduce the residual phase error in OFDM communication signals;

FIG. 7 is a flowchart describing a method for use in reducing the residual phase error in OFDM communication signals;

FIG. 8 is a timing diagram showing radio frequency (RF) OFDM
10 signals and OFDM packets in the wireless communication system;

FIG. 9 is an illustrative representation of the relationship between time slots and time frames utilized in the wireless communication system; and

FIG. 10 is an illustrative representation of the frequency layout of
15 traffic and pilot tones utilized in the wireless communication system.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1 is an illustrative representation of a wireless communication
20 system 100 which utilizes orthogonal frequency division multiplexing (OFDM) or OFDM-like communication methodologies. Wireless communication system 100 includes at least one base unit 106 having one or more antennas 108, and a plurality of remote units 102 ("RUs" or "transceiver units"), such as remote unit 104. Base unit 106 and remote
25 units 102 communicate via radio frequency (RF) signals, such as RF signals 110 between base unit 106 and remote unit 104. Wireless communication system 100 can make use of a number of different communication techniques, such as frequency division multiple access (FDMA), time division multiple access (TDMA), or time division duplex (TDD).

Preferably, wireless communication system 100 is a "fixed wireless system" (FWS) or Digital Broadband service, where base unit 106 provides telephone and high-speed data communication to each one of a number of fixed-location subscribers equipped with an RU. Also, the RF OFDM
5 communications signals are modulated using 16 quadrature amplitude modulation (QAM), or quadrature phase shift keying (QPSK). Further, the wireless system employs a frequency division duplex (FDD) technique to implement the downlink (base unit to remote unit) and uplink (remote unit to base unit) transmissions. Since uplink and downlink transmissions
10 are symmetric, only downlink transmission will be described herein.

Referring to FIG. 8, each base unit of the wireless communication system transmits a plurality of OFDM packets 802, such as an OFDM packet 804, to a corresponding remote unit. A new OFDM packet is transmitted once every predetermined time period. Each predetermined
15 time period is associated with a time slot, such as a time slot 906 of FIG. 9. As indicated in FIG. 9, a plurality of consecutive time slots 904 corresponds to a time frame 902. In the embodiment shown, each time slot has a duration of 375 microseconds, each OFDM packet is 320 microseconds in length, and each time frame corresponds to 8 time slots
20 for a duration of 3 milliseconds.

Each base unit transmits "traffic tones" and "pilot tones" to a corresponding remote unit. Traffic tones are utilized for the communication of voice and/or data, whereas pilot tones are utilized for channel compensation. In general, each remote unit samples the OFDM
25 waveforms at a sampling rate to generate time domain samples, and converts the time domain samples into frequency domain signals (e.g., traffic or pilot tones). Referring to FIG. 10, an illustrative representation of the frequency layout of traffic and pilot tones utilized in the wireless communication system is shown. Data symbols on traffic tones ("Tch") of
30 a particular frequency slot are transmitted in a particular time slot. For

example, data symbols on traffic tones 1002 of frequency slot 1006 are transmitted in one particular time slot. As indicated in FIG. 10, each frequency slot has eighteen traffic tones. One or more of these tones, such as a tone 1004, are used as pilot tones for channel estimation and compensation.

Each remote unit is assigned a traffic channel that is defined by a unique time and frequency slot combination. One remote unit may be assigned to receive information within, for example, each time slot t_0 (e.g., time slot 906 of FIG. 9) at frequency slot f_5 (e.g., a frequency slot 1002 of FIG. 10), while another remote unit may be assigned to receive information within, for example, each time slot t_6 at frequency slot f_2 . Each remote unit in the wireless communication system utilizes the pilot tone within its assigned time slot to perform channel compensation and the methods described herein. So, if a single pilot tone is provided within each time slot, then each remote unit utilizes a single pilot tone in each time frame for channel compensation.

FIG. 2 shows a general block diagram 200 of an OFDM-based radio communication system which utilizes pilot-based signal correction. Diagram 200 is divided into base unit processes 202 for a base unit, remote unit processes 204 for a remote unit, and an airlink 206. In base unit processes 202, binary information data is encoded using a channel encoding process 208 and mapped into M-1 multi-amplitude multi-phase constellation symbols using a signal mapping process 210. In a serial-to-parallel conversion process 212 ("S/P"), one pilot symbol is inserted in the information data sequence for a "user i" before its data is multiplexed with other users' data. There are total M symbols for user i. A data sequence of length N from K users is converted into N parallel symbols, which are fed into an Inverse Fast Fourier Transform (IFFT) 214 from a tone mapping process 214. IFFT 214 modulates these symbols on N subcarriers and sums them. Next, a guard interval is added by a guard interval insertion

process 218 and a parallel-to-serial conversion process 220 ("P/S") is applied. After digital-to-analog (D/A) conversion and filtering with a D/A converter and lowpass filter 222, the signals are upconverted to a carrier frequency and transmitted over airlink 206.

5 The signals over airlink 206 are received and processed by remote unit processes 204. After downconversion of the signals, lowpass filtering and analog-to-digital (A/D) conversion are applied using an A/D converter and lowpass filter 224. A serial-to-parallel conversion process 226 ("S/P") converts the signals from serial to parallel and a guard
10 interval removal process 228 removes the existing guard interval. Data for user i is demultiplexed from the output of a Fast Fourier Transform (FFT) 230, where tone demapping is performed by a tone demapping process 232. Pilot-based signal correction is performed using a channel estimation process 234 and a signal correction process 236. Finally, $M-1$ information-
15 bearing symbols are demapped and decoded into binary data by a signal demapping process 240 and a channel decoding process 242, respectively.

A collection of M consecutive sub-carriers/tones, called the transmission channel or link, is used to transmit M constellation symbols in a parallel fashion. The selection of M is based on the data rate and
20 fading environment. It is typically chosen so that the traffic transmission channel is frequency-flat and no channel equalizer is necessary. Therefore, the transmission channel of M sub-channels is assumed as a frequency-flat channel.

FIG. 3 shows a receiver processing portion 300 of a remote unit in
25 wireless communication system 100 of FIG. 1. Receiver processing portion 300 includes a channel estimation process 302 and a channel compensation process 304. The following detailed signal model analysis is based on receiver processing portion 300 shown in FIG. 3.

A block of M encoded and modulated constellation symbols to be
30 transmitted, denoted as $X(n)$, is

$$X(n) = \begin{bmatrix} S_1(n) \\ S_2(n) \\ \vdots \\ S_{M-1}(n) \\ S_P(n) \end{bmatrix} \quad (\text{Eq. 1})$$

where n is the index for the n th block of user data and each block consists of M symbols, one of them is the pilot symbol; $S_P(n)$ is the pilot symbol inserted in the n th block of user data; and $S_i(n)$, $i = 1, 2, 3, \dots, M-1$, are information-bearing symbols in the n th block of data.

Since the channel estimation and signal correction are conducted in every individual OFDM data block, the block index n in the remaining description will be ignored. Therefore, we have

$$X = \begin{bmatrix} S_1 \\ S_2 \\ \vdots \\ S_{M-1} \\ S_P \end{bmatrix} = \begin{bmatrix} X_{in} \\ S_P \end{bmatrix} \quad (\text{Eq. 2})$$

where the information-bearing data block, X_{in} , is

$$X_{in} = \begin{bmatrix} S_1 \\ S_2 \\ \vdots \\ S_{M-1} \end{bmatrix} = S \quad (\text{Eq. 3})$$

The transmission channel for an individual user is considered a frequency-flat fading channel and its transfer function is modeled as a complex coefficient denoted as $h(n)$. This is because the bandwidth which M subchannels spans is much less than the fading channel coherent bandwidth.

The receiver local oscillator (LO) phase noise has two effects on the OFDM signal. One effect is the common phase errors that are the same for all subchannels. The common phase error is, in fact, a phase shift for each subchannel and can be incorporated with fading channel phase. The second effect is a noise-like intercarrier interference (ICI). It can be treated as noise, and will therefore not be considered in the remaining description.

At the receiver side, the received signal may be represented as

$$r = \alpha \cdot X + N \quad (\text{Eq. 4})$$

15

and

where

$$\begin{bmatrix} r_1 \\ r_2 \\ \vdots \\ r_{M-1} \end{bmatrix} = \begin{bmatrix} \alpha \cdot S_1 + n_1 \\ \alpha \cdot S_2 + n_2 \\ \vdots \\ \alpha \cdot S_{M-1} + n_{M-1} \end{bmatrix}$$

and

$$r_{in} = \begin{bmatrix} r_1 \\ r_2 \\ \vdots \\ r_{M-1} \end{bmatrix} = \begin{bmatrix} \alpha \cdot S_1 + n_1 \\ \alpha \cdot S_2 + n_2 \\ \vdots \\ \alpha \cdot S_{M-1} + n_{M-1} \end{bmatrix} = \alpha \cdot X_{in} + N_{in} \quad (\text{Eq. 6})$$

$$N = \begin{bmatrix} n_1 \\ n_2 \\ \vdots \\ n_{M-1} \\ n_p \end{bmatrix} = \begin{bmatrix} N_{in} \\ n_p \end{bmatrix} \quad (\text{Eq. 7})$$

$$N_{in} = \begin{bmatrix} n_1 \\ n_2 \\ \vdots \\ n_{M-1} \end{bmatrix} \quad (\text{Eq. 8})$$

5 n_i , $i = 1, 2, 3, \dots, M-1$, and n_p are AWGN with a mean of zero and a variance of σ^2 . The received pilot symbol, r_p , is

Channel Estimation. Based on the received pilot symbol, r_p , in Eq. 9 and the previously known pilot symbol, S_p , and the channel transfer function, H , in the n th OFDM data block can be estimated based on

(Eq. 10)

$$\begin{aligned}
 \hat{\alpha} &= \frac{S_P^* \cdot r_P}{\|S_P\|^2} \\
 &= \alpha + \frac{S_P^* \cdot n_P}{\|S_P\|^2} \\
 &= \alpha + \alpha_N
 \end{aligned}$$

where α is the true fading channel gain or transfer function. The channel estimation error, α_N , due to co-channel interference (CCI), AWGN, and ICI is

5

$$\alpha_N = \frac{S_P^* \cdot n_P}{\|S_P\|^2} \quad (\text{Eq. 11})$$

Since S_p is a complex constant and its norm, $\|S_p\|^2$, is a real constant, the channel gain estimation error, ϵ_N , is an AWGN variable with a mean of zero and variance of $\sigma^2/\|S_p\|^2$. The mean-square-error (MSE) of the channel estimation method in Eq. 10 is

5

$$\text{MSE} = \sigma^2 / \|S_p\|^2 \quad (\text{Eq. 12})$$

$$\hat{\alpha} = (|\alpha| + \zeta) \cdot e^{j(\phi + \phi_N)} \quad (\text{Eq. 13})$$

FIG. 4 depicts the relationships between true channel gain (at 402), its estimate (at 404), and the estimation error (at 406). From FIG. 4, it is found that the estimated fading channel gain, $\hat{\alpha}$, can be given by

10 where ζ is a random variable and its value is limited as

$$-|\alpha| \leq \zeta < \infty \quad (\text{Eq. 14})$$

and ϕ_N is a phase error variable within a small range. The ϕ_N is the channel phase estimation error and it is called the residual phase error (at 408).

15

In Eq. 13, the real channel transfer function, α , in the n th OFDM block data, is treated as

(Eq. 15)

$$\alpha = |\alpha| e^{j\phi}$$

20 Signal Correction/Channel Compensation. With the estimate of fading channel gain or transfer function in Eq. 13, the received information bearing signals are corrected based on

$$\hat{x}_{in} = \frac{\hat{\alpha}^* \cdot r_{in}}{\|\hat{\alpha}\|^2} \quad (\text{Eq. 16})$$

Substituting r_{in} in Eq. 16 with the result in Eq. 6, Eq. 16 can be simplified as

$$\begin{aligned}
 \hat{X}_{in} &= \frac{\hat{\alpha}^* \cdot r_{in}}{\|\hat{\alpha}\|^2} \\
 &= \frac{\hat{\alpha}^* \cdot (\alpha \cdot X_{in} + N_{in})}{\|\hat{\alpha}\|^2} \\
 &= \frac{(\hat{\alpha}^* \cdot \alpha)}{\|\hat{\alpha}\|^2} \cdot X_{in} + \frac{\hat{\alpha}^* \cdot N_{in}}{\|\hat{\alpha}\|^2} \\
 &= \frac{|\alpha|}{\|\hat{\alpha}\|} \cdot e^{-j\phi_N} \cdot X_{in} + \frac{\hat{\alpha}^* \cdot N_{in}}{\|\hat{\alpha}\|^2} \\
 &= \frac{|\alpha|}{|\alpha| + \zeta} \cdot e^{-j\phi_N} \cdot X_{in} + \frac{\hat{\alpha}^* \cdot N_{in}}{\|\hat{\alpha}\|^2} \\
 &= \frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{-j\phi_N} \cdot X_{in} + S_N
 \end{aligned}
 \tag{Eq. 17}$$

where the second item of Eq.17 is due to CCI, AWGN, and ICI presented in information-bearing subchannels and it is given by

$$\begin{aligned}
 S_N &= \frac{\hat{\alpha}^* \cdot N_{in}}{|\hat{\alpha}|^2} \\
 &= \frac{\hat{\alpha}^*}{|\hat{\alpha}|^2} \cdot \begin{bmatrix} n_1 \\ n_2 \\ \vdots \\ n_{M-1} \end{bmatrix} \\
 &= \begin{bmatrix} S_{N1} \\ S_{N2} \\ \vdots \\ S_{NM-1} \end{bmatrix}
 \end{aligned} \tag{Eq. 18}$$

and

$$\hat{x}_{ia} = \begin{bmatrix} \hat{x}_1 \\ \hat{x}_2 \\ \vdots \\ \hat{x}_{M-1} \end{bmatrix} \tag{Eq. 19}$$

5

\hat{X}_i , $i = 1, 2, 3, \dots, M-1$ are estimates of constellation symbols transmitted over the fading channel using OFDM signals. These estimated symbols are then demodulated and decoded to the binary data.

Effect Of Channel Estimation Error, $\hat{\theta}_N$. An estimate for an individual symbol in the n th data block is given as follows:

$$\begin{aligned}\hat{X}_i &= \frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{-j\hat{\phi}_N} \cdot S_i + S_{Ni} \\ &= \frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{-j\hat{\phi}_N} \cdot S_i + \frac{\hat{\alpha}^*}{\|\hat{\alpha}\|^2} \cdot n_i\end{aligned}\quad (\text{Eq. 20})$$

The second item, S_{Ni} , is an AWGN variable. Eq. 20 reveals that the channel estimation error, $\hat{\theta}_N$, has two major effects on the transmitted symbols, S_i , $i=1, 2, 3, \dots, M-1$, in the n th block of OFDM data.

The first effect is that the constellation of transmitted symbols is scaled by a factor of

$$1/\left(1 + \frac{\zeta}{|\alpha|}\right)$$

instead of 1. If the channel estimation error is very small, or zero, then Eq. 20 becomes

$$\hat{X}_i = S_i + \frac{\hat{\alpha}^*}{\|\hat{\alpha}\|^2} \cdot n_i \quad (\text{Eq. 21})$$

However, if the channel estimation error is very large, or the channel gain, θ , is so small that the whole OFDM block signal is in deep fading and is immersed in the noise, the estimate, $\hat{\alpha}$, of the channel gain, θ , is almost zero and noise will only be obtained from the channel estimation and signal correction. Some diversities and combining techniques may be used to effectively deal with such deep fading in a wireless communication system.

The second effect is that the constellation of the transmitted symbols is rotated by an angle of $\hat{\phi}_N$. Similarly, if the channel estimation error is very small, then the residual angle will become small too. Both effects degrade the mean-square-error (MSE) performance of the received constellation signals at the input of the signal demapping and decoding

block. Furthermore, if a diversity and the maximum ratio combining (MRC) technique is employed at the receiver, the residual phase errors due to imperfect channel estimation in each branch will further degrade the overall system performance because the MRC requires co-phase
 5 signals from two branches of the receiver.

Residual Phase Error Estimation. The objective is to reduce the residual phase error in received constellation signals due to the pilot-based channel estimation. To reduce the effect of the channel phase estimation error on transmitted symbols, the channel phase estimation error must
 10 first be estimated and then removed from the received signals. What is described herein is a novel technique for estimating the residual phase error, ϕ_N , and utilizing it for such correction.

In Eq. 20, the received constellation symbol after the signal correction in the transfer domain is represented as

15

$$\begin{aligned}\hat{X}_i &= \frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{-j\phi_N} \cdot S_i + S_{Ni} \\ &= \frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{-j\phi_N} \cdot S_i + \frac{\hat{\alpha}^*}{|\hat{\alpha}|^2} \cdot n_i\end{aligned}\quad (\text{Eq. 22})$$

Using the similar method in deriving the Eq. 13, the Eq. 22 can be simplified as

$$\hat{X}_i = \left[\frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot |S_i| + \epsilon_i \right] \cdot e^{j(-\phi_N + \phi_i + \phi_{ni})} \quad i=1, 2, 3, \dots, M-1 \quad (\text{Eq. 23})$$

5 where ϕ_{ni} represents the effect of the second item in Eq. 22 on the amplitude of the i th transmitted symbol, S_i , and is a random variable and is confined within the following range:

$$\frac{1}{1 + \frac{\zeta}{|\alpha|}} \leq \epsilon_i < \infty \quad i=1, 2, 3, \dots, M-1 \quad (\text{Eq. 24})$$

and ϕ_{ni} is due to the second item in Eq. 22. It is a uniformly distributed
10 random phase variable within a small range and its mean is zero.

In simplifying Eq. 23, we used the expression

$$S_i = |S_i| e^{j\phi_i} \quad i=1, 2, 3, \dots, M-1 \quad (\text{Eq. 25})$$

where ϕ_i is the phase of the i th transmitted information symbol. The total
15 phase of the received signal, \hat{X}_i , is given as

$$\Phi_i = -\phi_N + \phi_i + \phi_{ni} \quad i=1, 2, 3, \dots, M-1 \quad (\text{Eq. 26})$$

and can be calculated based on

$$\Phi_i = \text{atan2}(\text{imag}(\hat{X}_i), \text{real}(\hat{X}_i)) \quad i=1, 2, \dots, M-1 \quad (\text{Eq. 27})$$

where atan2 is the four-quadrant inverse tangent and its output is in the
 5 interval $[-\pi, \pi]$; imag is the complex imaginary part; and real is the
 complex real part.

The first objective is to estimate the residual phase error, ϕ_N , from
 phases of the received signals in Eq. 26. It is found that the residual phase
 error, ϕ_N , is a constant for all $M-1$ received symbol signals. The phase
 10 errors, ϕ_{ni} , $i = 1, 2, 3, \dots, M-1$, in Eq. 26 are due to additive white Gaussian
 noise and are all random variables with a zero mean. These errors can be,
 for example, averaged out over $M-1$ received signal phases.

In order to estimate ϕ_N , it is important to know the information
 phase, ϕ_i , for each transmitted symbol, S_i . In the embodiment described, a
 15 hard-decision slicer is employed to find each transmitted symbol with a
 fair accuracy based on the corresponding received constellation signal.
 The output of the slicer is the estimate of the corresponding transmitted
 symbol at the transmitter end. Due to noise, co-channel interference, and
 channel estimation errors, the output of the slicer is given as

$$\begin{aligned} \hat{S}_i &= \text{Slicer}(\hat{X}_i) \\ &= \text{Slicer} \left[\frac{1}{1 + \frac{\zeta}{|\alpha|}} \cdot e^{j\phi_N} \cdot S_i + \frac{\alpha^*}{|\alpha|^2} \cdot n_i \right] \quad (\text{Eq. 28}) \\ &= \begin{cases} S_i & \text{(Right decision)} \\ S_j & \text{(Wrong decision), } i \neq j \end{cases} \end{aligned} \quad (\text{Eq. 28})$$

20

where S_i , and S_j , are transmitting constellation symbols. The
 corresponding information phase estimate, ϕ , is given as

$$\begin{aligned} \hat{\phi}_i &= \text{atan2}(\text{imag}(\hat{S}_i), \text{real}(\hat{S}_i)) \quad i=1, 2, \dots, M-1 \quad (\text{Eq. 29}) \\ &= \begin{cases} \phi_i & \text{(Right decision)} \\ \phi_j & \text{(Wrong decision), } i \neq j \end{cases} \end{aligned}$$

where, ϕ_i and ϕ_j , are the phases of transmitted symbols, S_i and S_j .

The symbol error is due to channel impairments and channel estimation errors. If the channel is very bad, the symbol error rate will be very high and therefore the slicer may not be reliable. In most situations, however, the symbol error rate is acceptable. For example, the symbol error rate is likely to be less than 5×10^{-2} when the slicer is employed in the embodiment described. That is, there may be one symbol error every 20 constellation symbols. Thus, for an OFDM-based system with the block size of 20, there may be one symbol error every OFDM data block. If the symbol error rate is 10^{-2} , then there may be one symbol error every 5 OFDM data blocks. As apparent, the slicer can be used to estimate the transmitted information symbol with an acceptable accuracy.

If no symbol error occurs in the slicer, the resulting phase error is given as

$$\begin{aligned} \Phi_{\text{err}}(i) &= \Phi_i - \phi_i \\ &= -\phi_N + \phi_{ai} \quad i=1, 2, 3, \dots, M-1 \end{aligned} \quad (\text{Eq. 30})$$

The estimate, $\hat{\phi}_N$, of the residual phase error, ϕ_N , due to channel impairments can be calculated by averaging the phase error in Eq. 30 over M-1 received symbols based on

$$\begin{aligned}\hat{\phi}_N &= -\frac{1}{M-1} \sum_{i=1}^{M-1} \Phi_{\text{err}}(i) \\ &= -\frac{1}{M-1} \sum_{i=1}^{M-1} (-\phi_N + \phi_{ai}) \\ &= \phi_N \frac{1}{M-1} \sum_{i=1}^{M-1} 1\end{aligned}\quad (\text{Eq. 31})$$

- 5 Since ϕ_{ai} , $i=1, 2, 3, \dots, M-1$, are random variables with zero means, the second item in Eq. 31 approaches zero when $M \gg 1$. As a result, the estimate of the residual phase error is

$$\hat{\phi}_N \equiv \phi_N \quad \text{if } M \gg 1 \quad (\text{Eq. 32})$$

- 10 Assuming that there is one symbol error and the j th transmitted symbol S_j is sliced as S_i in the n th OFDM block, then the total phase error for the j th received symbol is as follows:

$$\begin{aligned}\Phi_{\text{err}}(j) &= \phi_j - \phi_i \\ &= -\phi_N + \phi_{aj} + (\phi_j - \phi_i) \\ &= -\phi_N + \phi_{aj} + \Delta\end{aligned}\quad (\text{Eq. 33})$$

where

$$\Delta = \phi_j - \phi_i \quad i, j = 1, 2, \dots, M-1 \text{ and } i \neq j \quad (\text{Eq. 34})$$

If $\epsilon = 0$, the symbol error does not have any effect on the estimation
5 of the residual phase error using Eq. 31. Otherwise, we have

$$|\Delta| \geq \Delta_{\min} \quad (\text{Eq. 35})$$

where ϵ_{\min} is the minimum phase difference between two constellation
symbols if both symbols do not have the same phase. For instance, for a
16-QAM constellation, the $\epsilon_{\min} = \pi/8$, while for the QPSK constellation,
10 $\epsilon_{\min} = \pi/2$.

Therefore, an incorrect hard-decision or a symbol error results in
either a large or a small phase error for that symbol. If the maximum and
minimum values (i.e., largest of the absolute values) from M phase errors
in Eq. 30 are removed, and the remaining phase errors are averaged, the
15 effect of a symbol error on the estimation of the residual phase error will
be minimized. The estimate can be used to approximate the real residual
phase error as reflected by

$$\hat{\phi}_N \equiv \phi_N \quad \text{if } M \gg 1 \quad (\text{Eq. 36})$$

Statistically, if there are two symbol errors per OFDM data block, the first
two maximums and minimums (i.e., largest magnitudes) from M phase
20 errors are ignored. Since the size of cluster M is about 20, few symbol
errors do not significantly affect the estimation of the residual phase error.
In fact, it is rare that there are even a few symbol errors per OFDM block.

Once the residual phase error due to the channel estimation is
estimated, its effect on the received constellation signal is corrected or

compensated. Since this estimation method utilizes the detected symbols, it may be referred to as the data-directed residual phase error estimation (DD-RPEE) method. The correction or compensation method based on the DD-RPEE may be referred to as the data-directed residual phase error
5 correction (DD-RPEC) method.

Phase Error Reduction. A residual phase error estimator and corrector, that is, the DD-RPEE and the DD-RPEC previously derived, and an OFDM-based wireless receiver having the DD-RPEE and DD-RPEC, are depicted in FIG. 5. An alternative OFDM-based wireless receiver having
10 the DD-RPEE and DD-RPEC to reduce channel phase estimation error is depicted in FIG. 6. One or more processors may be utilized to perform the processes described, but preferably a single processor is utilized such as a single digital signal processor (DSP) to execute the appropriate steps.

More particularly, FIG. 5 shows a schematic block diagram of
15 receiver processing components 500 of a remote unit. Receiver processing components 500 include a channel estimation process 502, a channel compensation process 504, and a residual phase error (RPE) estimation process 506. Residual phase error estimation process 506 includes a phase calculation process 508 for channel-compensated data symbols, a symbol
20 slicer 510, a phase calculation process 512 for information symbols, a subtractor process 514, a maximum value removal process 516, an averaging process 518, and a signal correction process denoted at 520 and 522.

An alternate embodiment in FIG. 6 shows receiver processing
25 components 600 which include a channel estimation process 602, a channel compensation process 604, and a residual phase error (RPE) estimation process 606. Residual phase error estimation process 606 includes a phase calculation process 608 for channel-compensated data symbols, a symbol slicer 610, a phase calculation process 612 for information symbols, a
30 subtractor process 614, a maximum value removal process 616, an

averaging process 618, and a signal correction process denoted at 620, 622, and 624.

The DD-RPEE and DD-RPEC will now be described in relation to the flowchart of FIG. 7 and in connection with FIG. 5. The signal is first received (step 702 of FIG. 7 and point 550 of FIG. 5). Here, the n th block of M received symbols, $r(n)$ or r , is taken from outputs of the multiple access (FFT) block in the receiver at a time n . The n th received signal vector, r , is given in Eq. 5. Next, the fading channel gain is estimated (step 704 of FIG. 7 and channel estimation process 502 of FIG. 5). Here, the pilot tone symbol, r_p , in the n th received signal vector, r , is used to estimate the fading channel gain, $\hat{h} = |h|e^{j\phi}$. The channel estimate, $\hat{\alpha} = |\hat{\alpha}|e^{j\phi}$, is calculated based on Eq. 10. Next, the received signal, r_{inv} , is corrected or compensated (step 706 of FIG. 7 and channel compensation process 504 of FIG. 5). The n th received information-bearing data block of $M-1$ symbols, r_{inv} , was corrupted by the fading channel gain and noise. Step 706 corrects or compensates the signal vector, r_{inv} , with the channel estimate, $\hat{\alpha} = |\hat{\alpha}|e^{j\phi}$, from step 704, based on Eq. 16. The output signal vector, \hat{X}_{in} , is given in Eq. 16, and it contains $M-1$ compensated information-bearing tone symbols which are corrupted by the channel estimation errors including channel residual amplitude and phase errors and noise.

The "core" of the phase error estimation begins in the next step. The phase of signal vector, \hat{X}_{in} , is calculated (step 708 of FIG. 7 and phase calculation process 508 of FIG. 5). Here, the signal vector, \hat{X}_{in} , has $M-1$ data symbols and the phase, ϕ_i , $i = 1, 2, 3, \dots, M-1$, of each symbol is calculated based on Eq. 26. Next, the transmitted symbols are estimated (step 710 of FIG. 7 and symbol slicer 510 of FIG. 5). In this step, a hard-decision is made for each element of signal vector, \hat{X}_{in} , to estimate its corresponding information symbol, $X_i = S_i$ (where $i = 1, 2, 3, \dots, M-1$). The

hard-decision is implemented by a corresponding constellation slicer. If no decision error occurs, the output is the symbol transmitted from the transmitter; otherwise, the output is an incorrect symbol. Next, the phases of each estimated information symbol are estimated (step 712 of FIG. 7 and phase calculation process 512 of FIG. 5). Here, the phase of the estimated information symbol, \angle_i (where $i = 1, 2, 3, \dots, M-1$), is calculated based on Eq. 29. Next, the information phase is subtracted from the total received signal phase (step 714 of FIG. 7 and subtractor process 514 of FIG. 5). For execution of this step, the total signal phase was given in step 708 and the phase of its estimated information symbol was given in step 712. The difference, $\phi_{\text{err}}(i)$ $i = 1, 2, 3, \dots, M-1$, between the total phase of the received signal and the phase of its corresponding estimated information symbol is calculated based on Eq. 28. If a symbol is detected with an error, the resulting phase difference is relatively large.

Next, the largest magnitude phase error is removed (step 716 of FIG. 7 and maximum value removal process 516 of FIG. 5). As previously described, the largest magnitude phase error corresponds to a symbol detection error. Removing the largest magnitude phase difference from $M-1$ phase difference variables, $\phi_{\text{err}}(i)$ $i = 1, 2, 3, \dots, M-1$, will result in an unbiased estimate of phase error. Therefore, only $M-2$ phase difference variables are left for next step processing. It is noted that any suitable number of maximum values may be removed. Next, the phase differences are averaged (step 718 of FIG. 7 and averaging process 518 of FIG. 5). There are total of $M-2$ phase difference variables from step 716, and the average is performed over $M-2$ variables based on Eq. 29. The mean or the output of averaging process 518 is the estimate of the residual phase error. Finally, the signal vector, \hat{X}_m , is corrected or compensated (step 720 of FIG. 7 and blocks 520 and 522 of FIG. 5). In FIG. 5, the residual phase error in each element of the signal vector, \hat{X}_m , is removed by multiplying the

received signal with the estimated residual phase error. The output will be the "clear" signal.

The channel estimate may need to be corrected (step 722 of FIG. 7 and block 622 of FIG. 6).¹ For the alternative/extended version shown in FIG. 6, the channel estimate, $\hat{\alpha} = |\hat{\alpha}|e^{j\hat{\phi}}$, is first compensated with the estimated residual phase error, $\hat{\phi}$, based on the following equation, and then the corrected channel estimate, $\tilde{\alpha}$, is used to correct or compensate (block 624 of FIG. 6) the received signal vector, \hat{X}_m , by repeating step 720:

$$\tilde{\alpha} = \hat{\alpha} \cdot e^{-j\hat{\phi}} \quad (\text{Eq. 37})$$

10 The received signal is then demodulated/decoded (step 724). The corrected received signal, based on the output of steps 720 and 722, is fed to demodulation and decoding blocks to retrieve transmitted information bits.

It should be readily apparent and understood that the foregoing description is only illustrative of the invention and in particular provides preferred embodiments thereof. Various alternatives and modifications can be devised by those skilled in the art without departing from the true spirit and scope of the invention. Accordingly, the present invention is intended to embrace all such alternatives, modifications, and variations which fall within the scope of the appended claims.

20 What is claimed is:

CLAIMS

1. A method for use in reducing a residual phase error in orthogonal frequency division multiplexed (OFDM) communication signals, the method comprising:
 - 5 calculating a phase of each one of a plurality of channel-compensated data symbols to generate a plurality of data symbol phases;
 - performing a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols;
 - calculating a phase of each one of the plurality of information
 - 10 symbols to generate a plurality of information symbol phases;
 - calculating a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences; and
 - determining a residual phase error based on the plurality of phase
 - 15 differences.
2. The method according to claim 1, further comprising:
 - correcting phases of channel compensated data symbols based on
 - the determined residual phase error.
 - 20
3. The method according to claim 1, further comprising:
 - correcting phases of OFDM communication signals based on the
 - determined residual phase error.
 - 25
4. The method according to claim 1, further comprising:
 - prior to calculating each data symbol phase and generating each
 - information symbol, performing channel compensation on OFDM
 - communication signals using a pilot tone symbol received in the OFDM
 - communication signals to generate the plurality of channel-compensated
 - 30 data symbols.

5 5. The method according to claim 1, wherein determining the residual phase error comprises determining the residual phase error without considering one or more of the largest magnitudes in the plurality of phase differences.

 6. The method according to claim 1, further comprising:
 using the one or more phase differences to generate an average phase difference; and
10 wherein determining the residual phase error comprises determining the residual phase error based on the average phase difference.

 7. The method according to claim 1, further comprising:
15 disregarding one or more of the largest magnitudes in the plurality of phase differences in selecting the one or more phase differences;
 using the one or more phase differences to generate an average phase difference;
 wherein determining the residual phase error comprises
20 determining the residual phase error based on the average phase difference; and
 correcting phases of channel compensated data symbols based on the determined residual phase error.

25 8. A method for use in reducing a residual phase error in orthogonal frequency division multiplexed (OFDM) communication signals, the method comprising:
 generating a plurality of channel-compensated data symbols by performing channel compensation on OFDM communication signals using
30 one or more pilot tones;

calculating a phase of each one of the plurality of channel-compensated data symbols to generate a plurality of data symbol phases;

performing a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols;

5 calculating a phase of each one of the plurality of information symbols to generate a plurality of information symbol phases; and

calculating a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences.

10

9. The method according to claim 8, further comprising:

selecting a subset of phase differences from the plurality of phase differences that do not include one or more of the largest magnitudes in the plurality of phase differences;

15 using the subset of phase differences to generate an average phase difference;

determining a residual phase error based on the average phase difference; and

20 correcting phases of channel compensated data symbols based on the determined residual phase error.

10. The method according to claim 8, wherein calculating the phase is based on a four-quadrant inverse tangent function.

25 11. A residual phase error (RPE) correction apparatus for orthogonal frequency division multiplexed (OFDM) communication signals, comprising:

30 a first phase calculator to calculate a phase of each one of a plurality of channel-compensated data symbols to generate a plurality of data symbol phases;

a slicer to perform a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols;

5 a second phase calculator to calculate a phase of each one of the plurality of information symbols to generate a plurality of information symbol phases;

a phase difference calculator to calculate a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences; and

10 a residual phase error estimator to determine a residual phase error based on one or more of the plurality of phase differences.

12. The RPE correction apparatus according to claim 11, further comprising:

15 a phase corrector to correct phases of channel compensated data symbols based on the determined residual phase error.

13. The RPE correction apparatus according to claim 11, further comprising:

20 a phase corrector to correct phases of OFDM communication signals based on the determined residual phase error.

14. The RPE correction apparatus according to claim 11, further comprising:

25 a channel compensator to perform channel compensation on OFDM communication signals using a pilot tone symbol received in the OFDM communication signals to generate the plurality of channel-compensated data symbols.

15. The RPE correction apparatus according to claim 11, wherein said residual phase error estimator is further operative to determine the residual phase error without considering one or more of the largest magnitudes in the plurality of phase differences.

5

16. The RPE correction apparatus according to claim 11, further comprising:

a phase difference averager to use the one or more phase differences to generate an average phase difference; and

10 wherein said residual phase error estimator is further operative to determine the residual phase error based on the average phase difference.

17. The RPE correction apparatus according to claim 11, wherein one or more processors comprise said first and said second phase
15 calculators, said phase difference calculator, and said residual phase error estimator.

18. A residual phase error (RPE) correction apparatus, comprising:

20 a channel compensator to generate a plurality of channel-compensated data symbols by performing channel compensation on orthogonal frequency division multiplexed (OFDM) communication signals using one or more pilot tones;

a first phase calculator to calculate a phase of each one of the
25 plurality of channel-compensated data symbols to generate a plurality of data symbol phases;

a slicer to perform a hard-decision on each one of the plurality of channel-compensated data symbols to estimate a plurality of information symbols;

a second phase calculator to calculate a phase of each one of the plurality of information symbols to generate a plurality of information symbol phases; and

5 a phase difference calculator to calculate a phase difference between each data symbol phase and its associated information symbol phase to generate a plurality of phase differences.

19. The RPE correction apparatus according to claim 18, further comprising:

10 a selector to select a subset of phase differences from the plurality of phase differences that do not include one or more of the largest magnitudes in the plurality of phase differences;

an averager to use the subset of phase differences to generate an average phase difference;

15 a residual phase error estimator to determine a residual phase error based on the average phase difference; and

a phase corrector to correct phases of channel-compensated data symbols based on the determined residual phase error.

20 20. The RPE correction apparatus according to claim 18, wherein said second phase calculator is further operative to calculate the phase based on a four-quadrant inverse tangent function.

21. A method for use in reducing a residual phase error in
25 communication signals, the method comprising:

generating a plurality of channel-compensated data symbols by performing channel compensation on communication signals using one or more pilot tones; and

30 correcting phases of channel compensated data symbols based on hard-decisions of the plurality of channel-compensated data symbols.

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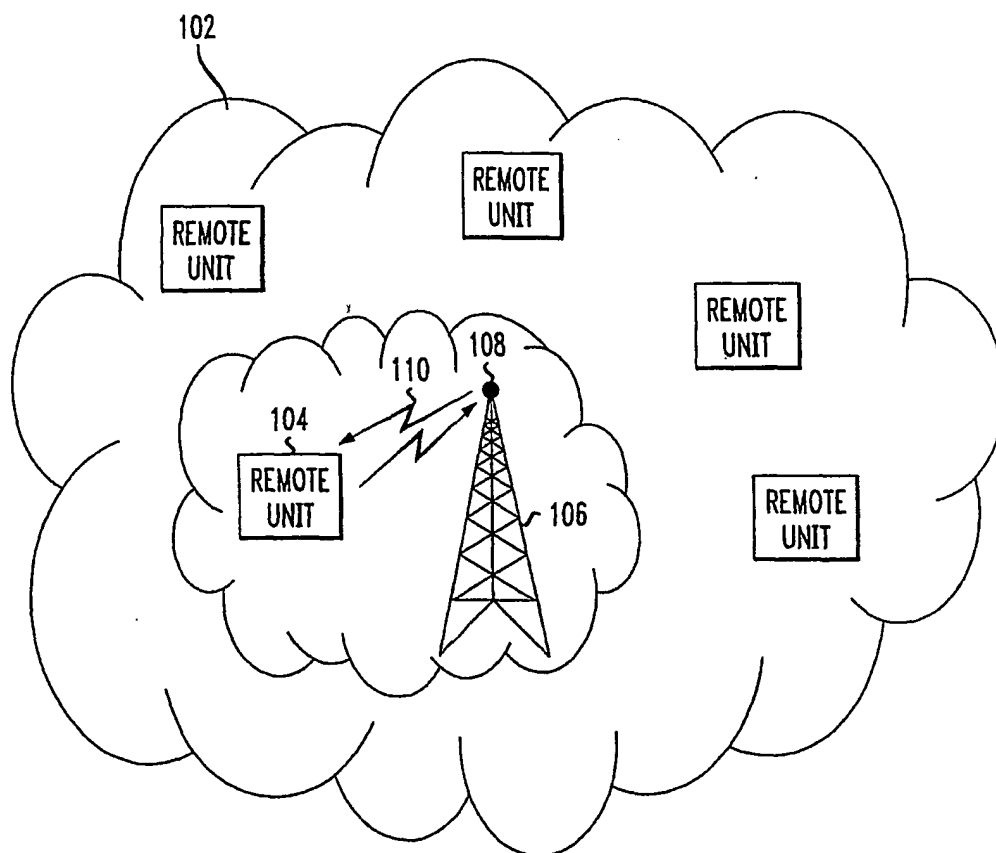
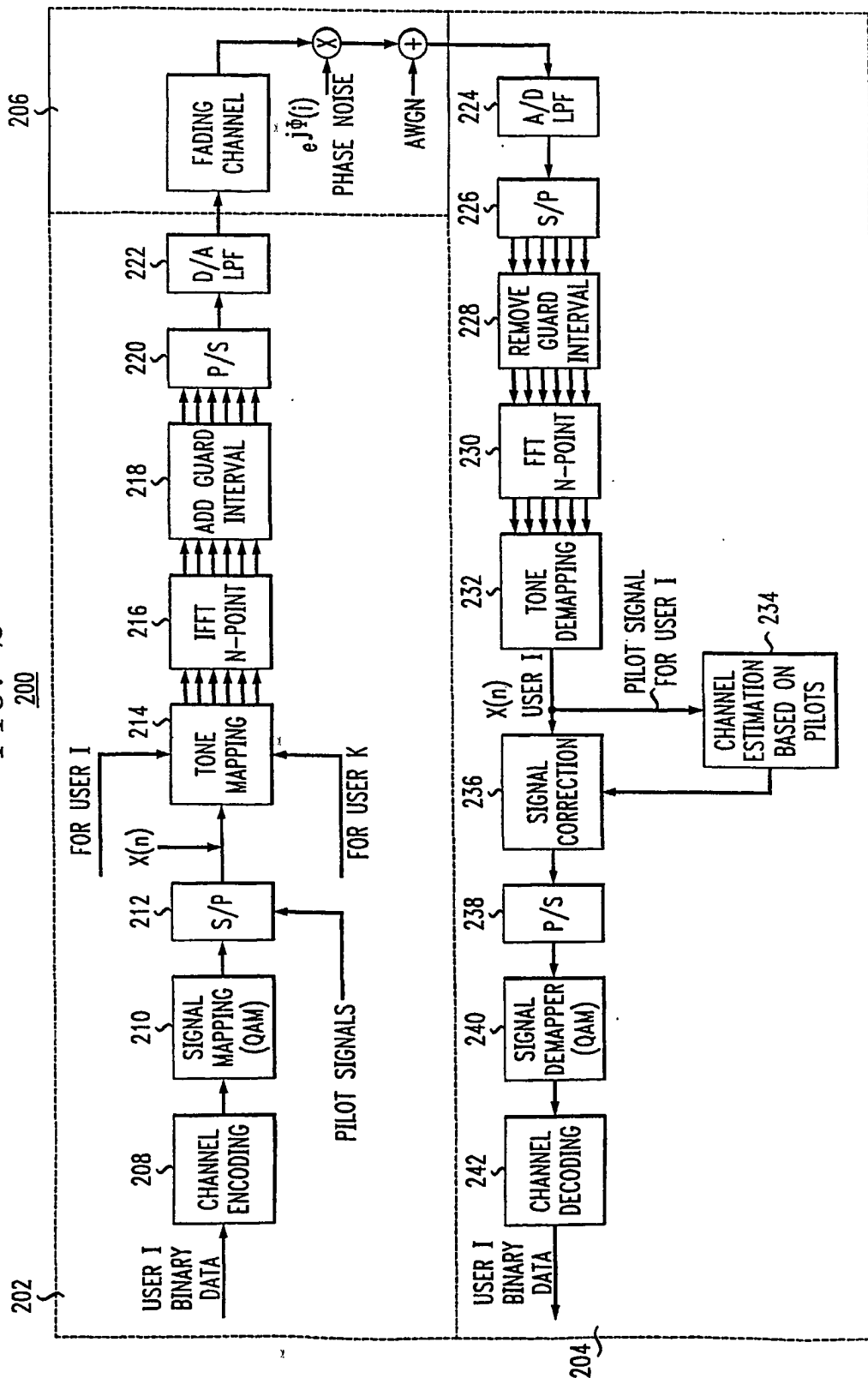
*FIG. 1*100

FIG. 2



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FIG. 3

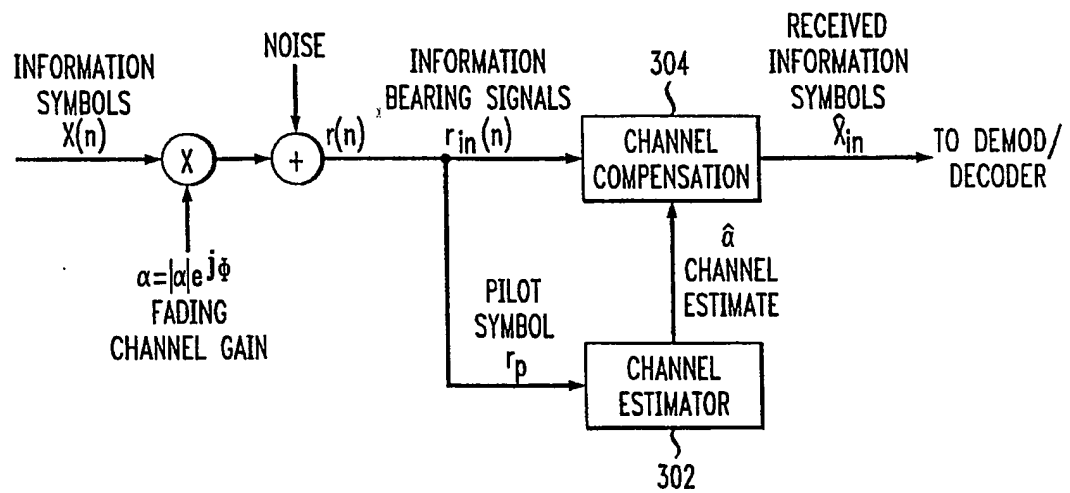
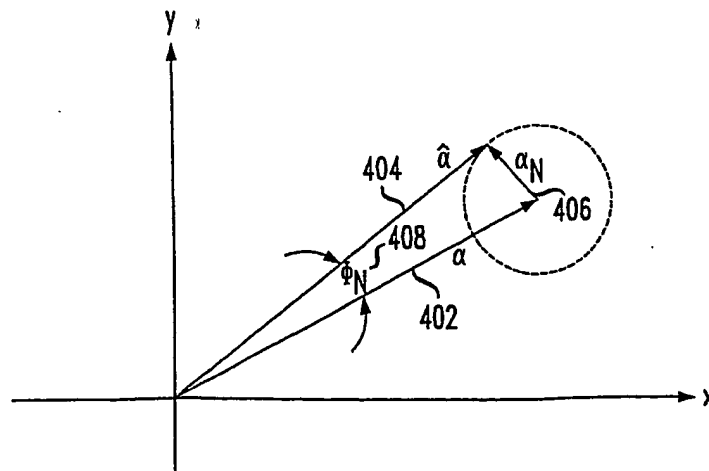
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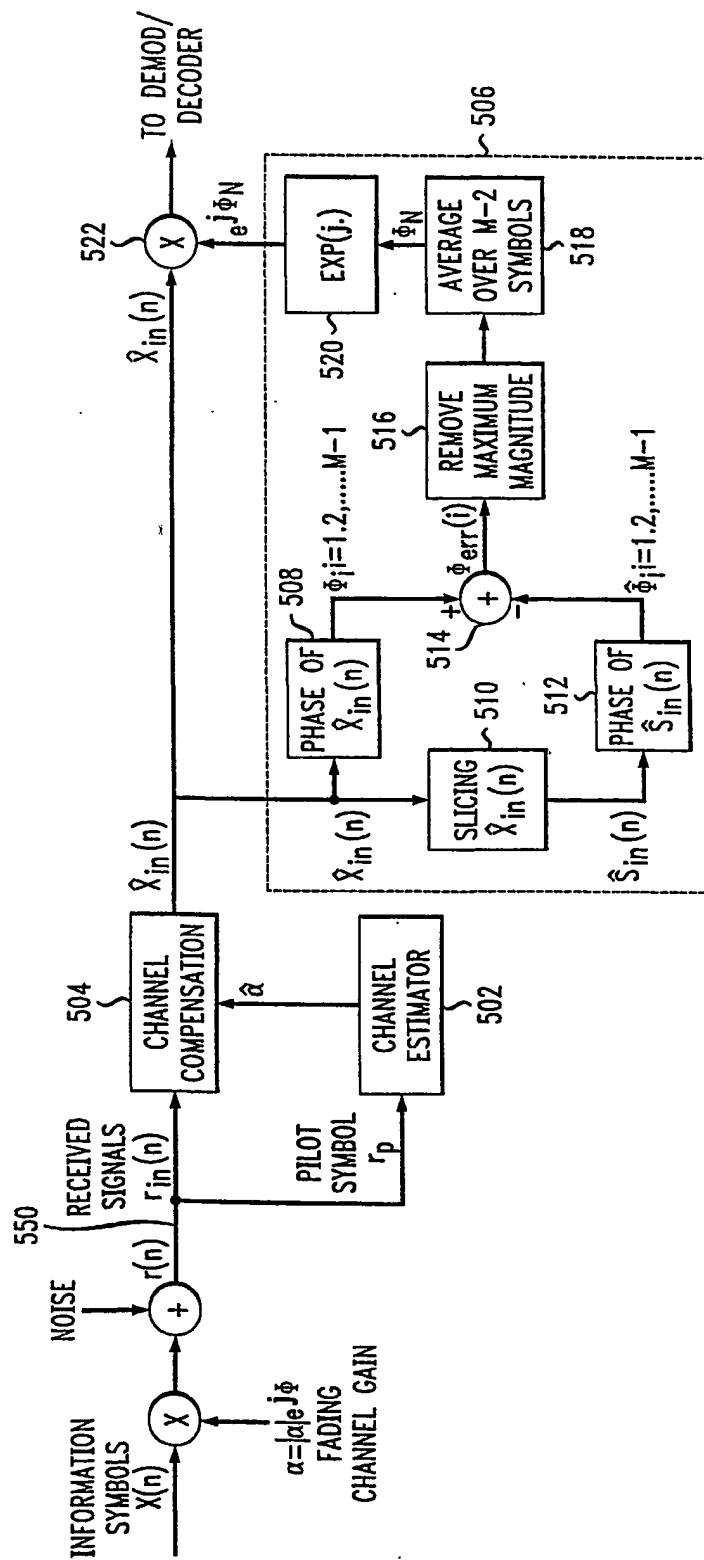
FIG. 4

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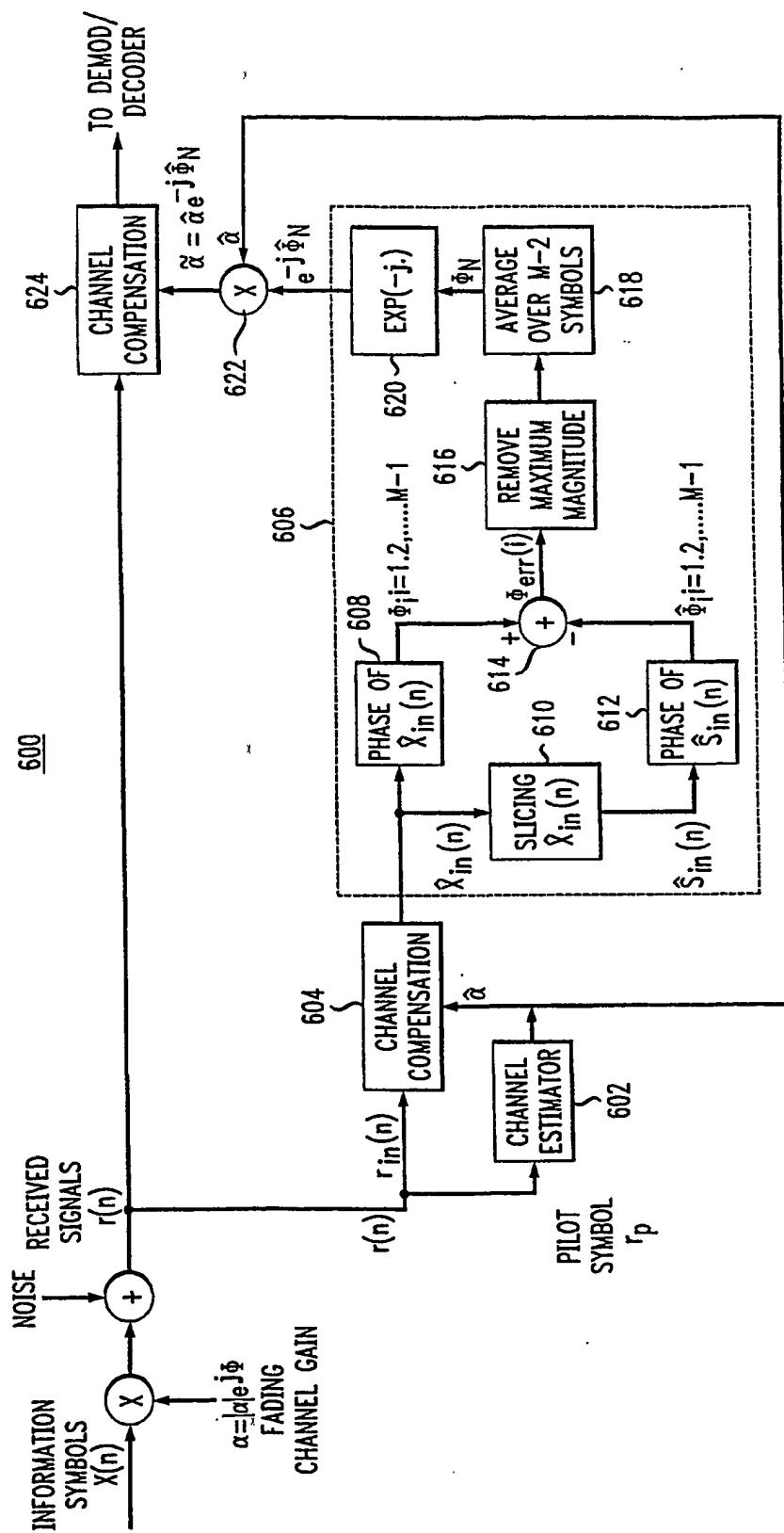
FIG. 5

500



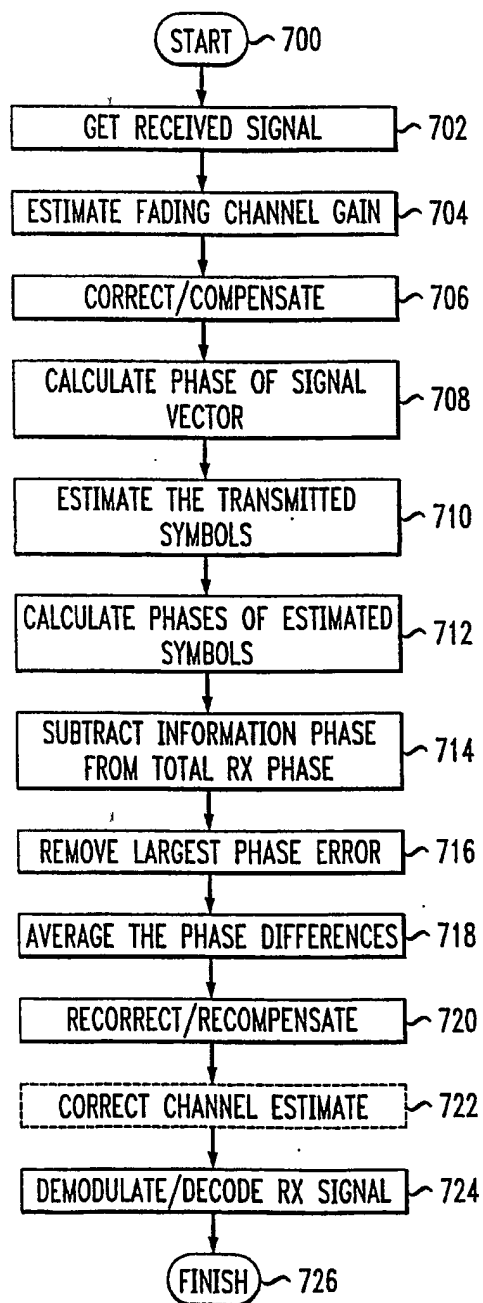
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FIG. 6



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FIG. 7



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FIG. 8

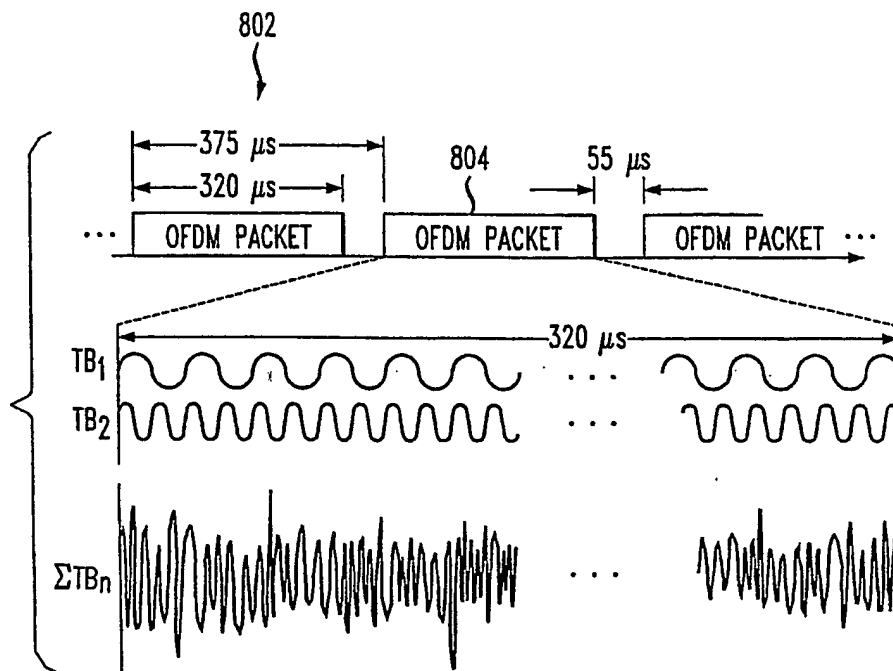


FIG. 9

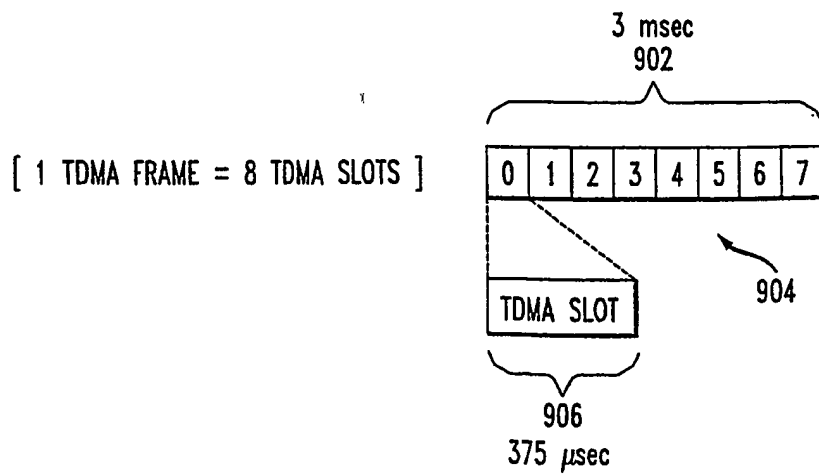


FIG. 10

